

02 | 2023

CIMAC Guideline

Used engine oil analysis

This publication is for guidance and gives an overview regarding the ... [e.g. risks inherent to the development and design of specific machinery]. The publication and its contents have been provided for informational purposes only and is not advice on or a recommendation of any of the matters described herein. CIMAC makes no representations or warranties express or implied, regarding the accuracy, adequacy, reasonableness or completeness of the information, assumptions or analysis contained herein or in any supplemental materials, and CIMAC accepts no liability in connection therewith.

Content

1	Reasons for doing used oil analysis	3
2	What, when, and how to sample	3
2.1	When to sample	4
2.2	How to sample	4
3	Interpretation of results and actions to take	4
3.1	4-stroke engine – used engine oil analysis	5
3.2	2-stroke engine – used system oil analysis	7
3.3	2-stroke engine – scrape down oil analysis	10
4	Shore laboratory based analysis versus ship board analysis methods	11

1 Reasons for doing used oil analysis

The key reason for doing USED OIL ANALYSIS (UOA) is to ensure machinery condition is effectively monitored over time thereby avoiding expensive machinery failures. Machinery failures at sea can be disastrous and USED OIL ANALYSIS is critical tool in helping ensure machinery provides continuous reliable service. USED OIL ANALYSIS can be likened to a health check for machinery. It allows early detection of wear and the condition of the lubricant and its suitability for continued service.

Oil analysis can monitor equipment condition before damage occurs. This includes the ability to monitor lubricant condition and the presence of contaminants and moisture. A huge benefit of oil analysis is to detect problems in both the oil and the machine. The many benefits of routine used oil analysis include:

- Longer equipment life. Oil analysis ensures machinery is being optimally lubricated while also monitoring issues such as wear and contamination
- Extend lubricant life. Oil analysis yields a clear picture of the condition of the lubricant so that it does not have to be changed prematurely
- Reduce equipment downtime. Oil analysis gives maintenance personnel the opportunity to detect and correct issues before a failure or breakdown occurs, thereby reducing the potential for serious disruptions in operations

2 What, when, and how to sample

The following table lists typical ship board equipment that can benefit from Used Oil Analysis monitoring:

Table 1: Marine Applications for UOA

Typical marine application for Used Oil Analysis	
Main Engines	Purifiers
Auxiliary engines	Reduction Gears
Cam shaft systems	Slow-speed engines system oil
Compressors (air/refrigeration/cargo)	Steering gear hydraulic gears
Deck gear drives	Control Pitch Propeller (CPP) System
Deck hydraulics	Thrusters
Gas Turbines	Stern tube
Thermal Oil system	

NOTE: The scope of this paper is limited to Used Engine Oil Analysis

2.1 When to sample

The goal of sample frequency is to achieve a regular pattern of sampling. This establishes a credible historical trend of machine and oil performance.

- Follow OEM-recommended sample intervals for your equipment.
- Follow classification societies' guidelines, such as DNV, Lloyd's Register and ABS.
- In the absence of OEM guidelines, refer to the recommendations below for general guidance in establishing initial sample frequency.
 - Low Speed Engine system oil.... (1000 to 2000 hours)
 - Low Speed Engine scrape down oil.... after reaching high load, after every fuel change, and after changing oil feed rate setting. Refer to OEM recommendation
 - Medium Speed Engine..... (500 to 1000 hours).
 - High Speed Engine..... (250 to 500 hours)

2.2 How to sample

Each sample has to be representative.

To obtain accurate analysis:

- Always flush sampling point before taking sample.
- Sample at consistent intervals from the correct sample location using proper sampling techniques¹. In addition, periodic sampling should be done from the same location and in the same procedure.
- Sample at operating temperature through a sampling valve, vacuum pump or sampling tube. Be safe, use caution when oil is above 120°F (50°C). Use protective gear recommended in the Safety Data Sheet for the lubricant.
- Use clean sample bottles and sampling point. The sampling should be carried out in a clean environment and the bottle should be sealed and labelled immediately after filling.
- Record equipment and sample details. Document this data to improve interpretation and establish an analysis trend.
- Obtain fresh oil sample for a baseline
- Drain and fill sample must be taken

3 Interpretation of results and actions to take

Interpreting the results from Used Oil Analysis is key. The following sections provide guidance with respect to different machinery types.

¹ Refer to CIMAC Recommendation 30 for details of sampling best practices.
Refer to OEM literature for recommended sample points, frequency, and technique.

3.1 4-stroke engine – used engine oil analysis

Interpretation of the used oil analysis is closely linked to the following variables:

- Type of fuel burned by the engine, namely, E.g. distillate fuel, residual fuel, bio-fuel, gas or other.
- The quality and performance of the lubricating oil and it's treatment system (purification, separation – temperature setting, and filtration – absolute mesh size)
- Engine design, for example, the following conditions increase oil stress... increased firing pressure, increased engine or oil temperature, reduced oil capacity and low oil consumption.
- Operating variables such as how long oil has been in service, high or low load engine operation.

The following table is a guide showing suggested parameters to measure in 4-Stroke Engine Oil Analysis and a brief interpretation of the results.

Table 2: 4 Stroke Engine Oil Analysis Interpretation

Parameter	Change	Possible Reason	Potential Risk
Primary			
Viscosity	Increase	Residual fuel ingress Asphaltenes Oil ageing / Oxidation Contamination Additive degradation Inadequate purifier operation High soot Incorrect oil grade used Emulsion (water)	Increase in friction Temperature rise Bearing damages Deposits
Viscosity	Decrease	Distillate fuel dilution Oil shear Incorrect oil grade used	Bearing damages
BN	Increase	Top up with high BN oil	Increased piston top land and exhaust valve deposits
BN	Decrease	High Sulphur fuel impact (Neutralizing acids)	Cylinder component corrosion Deposits
Water Content	Increase	Cooling water leakage Condensation Incorrect purifier setting	Corrosion Bearing damage Sludge deposits

			Filter blockage
Flash Point	Decrease	Distillate fuel dilution	Reduction in viscosity bearing damage
Insolubles	Increase	Residual fuel ingress Asphaltenes Oil ageing / Oxidation Contamination Wear debris Extended oil drain interval Inadequate purifier operation	Viscosity increase causing increased friction Bearing damage Accelerated Wear Filter blockage Deposits Formation of sludge
More Detail			
Soot	Increase	Poor combustion Oil ageing Insufficient purification or filtration	Increased engine wear Deposits or sludge
Asphaltenes	Increase	Combustion residue (residual fuels) Residual fuel leakage	Deposits Sludge formation Viscosity increase
Oxidation	Increase	Oil ageing Overheating Blow by	Viscosity increase Deposits BN reduction Insoluble increase Oil filter blockage Corrosion of metal parts and increased component wear
Nitration	Increase	High temperature NOx production and reaction with oil	Viscosity increase and deposits
TAN	Increase	Oil ageing Oil oxidation Contamination	Accelerated oil ageing Corrosion of metallic components Additive depletion Viscosity increase
Wear elements * Fe, Cr, Al, Pb, Sn, Cu	Increase	Wear of bearings, piston rings, cylinder liners	Damage to respective engine components depending on the wear elements found

		and other engine components	
Common additive elements Ca, Si, P, Zn, Mg	Decrease	Some consumption of additives is acceptable Dilution with incorrect oil grade	Only for trending
Contamination ** Na, Ni, V, Al, Si, Cl, Mg, B, K	Increase	Sea water ingress Cooling water ingress Fuel ingress	Only for trending

* Trending the oil analysis results with historical data is a very effective way of interpreting the results. For example, minor presence of Fe or Cu may not be a cause of concern if the presence is consistent with the history of previous analyses.

** K, Mg, B, Cl and Na derive from water-based contaminants, condensate, sea water, coolant etc. Si may come from dust/sand (e.g. Aluminum Silicate) but is typically also contained in lubricating oil additives (anti-foam). Presence of V and Ni are derived from residual fuel and is indicative of fuel oil contamination. Na and K can derive from heavy fuel oil and diesel fuels containing biodiesel or can be present from additives used in the engine coolant.

NOTE: It's the trend in the above measurements that is most important. Any change in trend has to be investigated. Failure to do this investigation completely negates the value of used oil analysis.

The above guide is just a brief summary. For more detailed information on 4-stroke engine oil analysis and interpretation, see CIMAC Recommendation 29 for medium speed engines and CIMAC Recommendation 20 for high-speed engines.

3.2 2-stroke engine – used system oil analysis

System oils provide the following functions: bearing lubrication, piston cooling, gear lubrication, and serve as a hydraulic fluid.

System oils should not form an emulsion because this will prevent the centrifuge from removing water.

Performance of the lubricating oil treatment system (purification, separation, and filtration) will have a big impact on the suitability of the lubricating oil.

Issues that deteriorate system oil performance include: High leakage of scrape down oil through piston rod stuffing box, water contamination, and contamination with fuel.

More detailed information on system oil analysis and interpretation can be found in CIMAC Recommendations 30 and 31.

The following table is a guide to which parameters to measure in 2-Stroke System Oil Analysis and a brief interpretation of the results

Table 3: Two Stroke Engine Oil Analysis Interpretation

Parameter	Change	Possible Reason	Potential Risk
Primary			
Viscosity	Increase	Stuffing Box leakage Oil ageing / Oxidation Residual fuel contamination Inadequate purifier operation Incorrect oil grade used	Increased bearing friction Deposits (piston cooling space, bearings)
	Decrease	Stuffing box leakage Distillate fuel contamination	Bearing failure
BN	Increase	Stuffing box leakage Different oil grade added	Impacts water separation
BN	Decrease	Incorrect oil grade used	Corrosion Crankcase deposits
Water Content	Increase	Cooling water leakage Water ingress (FW/SW) Condensation Inadequate purifier operation	Corrosion Acid formation Reduce additive effectiveness Bearing damage Sludge deposits Hydraulic system failure Filter blockage
Flash Point	Decrease	Distillate fuel dilution from leaky fuel pumps	Viscosity decrease Poor lubrication Crankcase explosion
Insolubles	Increase	Residual fuel ingress Wear debris Oil degradation Inadequate purifier operation	Viscosity increase Accelerated wear Filter blockage Deposits Sludge
More Detail			

Particle Count	Increase	Stuffing box seal leakage Wrong/incorrect sampling procedure/location Inadequate purification Wear particles Fuel contamination Fresh oil top up	Increased wear of bearings, etc. Damage to hydraulic system components
*Wear elements Fe, Cr, Al, Pb, Sn, Cu	Increase	Wear of bearings, journals, gears, stuffing boxes, and other engine components	Look for wear of respective engine components based on trend analysis for wear elements
**Common additive elements Ca, Si, P, Zn, B, Mg	Decrease or Increase	Different oil added Stuffing box leakage Extended oil usage causes depletion Inadequate purifier operation	Follow trends. The additives are used to enhance oil properties such as anti-wear, corrosion inhibitor, detergent, rust inhibitor, anti-friction, and antioxidants
**Contamination Ni, V, Na, K, Mg, B, Cl	Increase	Sea water ingress Cooling water ingress Fuel ingress	Follow trend

* Trending the oil analysis results with historical data is a very effective way of interpreting the results. For example, minor presence of Fe or Cu may not be a cause of concern if the presence is consistent with the history of previous analyses.

** K, Mg, B, Cl and Na derive from water-based contaminants, condensate, sea water, coolant etc. Si may come from dust/sand (e.g. Aluminum Silicate) but is typically also contained in lubricating oil additives (anti-foam). Presence of V and Ni are derived from residual fuel and is indicative of fuel oil contamination. Na and K can derive from heavy fuel oil and diesel fuels containing biodiesel or can be present from additives used in the engine coolant.

NOTE: It's the trend in the above measurements that is most important. Any change in trend has to be investigated. Failure to do this investigation completely negates the value of used oil analysis.

Best practice involves establishing a historical baseline and watching for a significant change or trend. Plotting the results is the best way to see changes and gauge their significance. A correct interpretation is based on your historical database or the recommendations of the engine builder.

3.3 2-stroke engine – scrape down oil analysis

The following table is a guide to which parameters to measure in 2-Stroke Scrape-Down Oil Analysis and a brief interpretation of the results

Table 4: 2 stroke engine scrape down oil sample interpretation

Parameter	Change	Possible Reason	Potential Risk
Primary			
BN	Too Low	Cylinder oil BN or feed rate too low for fuel sulfur content	Cold corrosion/wear Increased ring land and pack deposits
	Too high	Cylinder oil BN or feed rate too high for fuel sulfur content	Increased piston top land and crown deposits Possible liner polish Possible scuffing Deposits on Exhaust systems
Water Content	Increase	Inefficient water catchers Cooling water leakage	Corrosive wear
Wear elements Fe, total iron	Over OEM limit	Corrosive and mechanical wear of rings and liner Low cylinder oil feed rate	Abnormally high wear See notes below*
Fe, metal particles	Increase	Mechanical wear of rings and liner Low cylinder oil feed rate	Abnormally high wear See notes below*
Cr, Mo, Cu, Al, Si, Va	Increase	Stuffing box wear Ring wear Wear of piston skirt Cat fines from fuel Poor combustion	Abnormally high wear

* Concentration of ferrous iron in the scrape down oil is indicative of engine liner wear due to abrasion. The level of iron salts in the sample is an indication of engine liner wear due to corrosion.

Scrape Down oil sample composition can vary greatly from cylinder-to-cylinder and over time. As a result, a database of many past samples is required before you can interpret present results. Expect changes in fuel Sulphur level and load to have big effects.

A Sweep Test or Piston Underside Drain Oil Analysis Test should be carried out to optimize the cylinder oil feed rate based on the iron and BN levels. Refer to individual OEM latest guidelines for details of method.

Obtaining a representative sample is key criteria for attaining correct analysis and interpretation.

[Reference: Study of the relationship between cylinder lubricant drain condition and performance parameters of 2-stroke cross-head engines. (Congress 2001, Hamburg)]

[Reference: Investigations into abrasive and corrosive wear mechanisms of pistons and liners in large bore 2-stroke diesel engine cylinders. (Paper no. 14: CIMAC Congress 2004, Kyoto)]

4 Shore laboratory based analysis versus ship board analysis methods

There are currently many test kits, methods, and on-line sensors available for analyzing used oil on board the vessel. They are continually being developed and refined and this paper does not attempt to catalog them or compare them. Instead, the operator can compare and utilize shipboard analyses along with laboratory analysis.

Shore laboratory analyses benefit from very sophisticated equipment, highly trained analysts, and elaborate ways of checking the accuracy. This is impossible to duplicate in ship board analysis methods. On the other hand, a shore laboratory analysis can at times suffer delay due to the time required to get samples from the ship to a shore laboratory. The advantage of the onboard test is that it can give quick results allowing the ship staff to take immediate action.... before the shore results become available. The onboard tests, especially when the results are abnormal, should be backed up with shore analysis.

The operator must develop trust in a shipboard analysis. This can be done by running analyses of duplicate samples, one at the shore lab, and the other using the shipboard analysis. The results can be used to develop a comparison database and then periodically carrying out the duplicate analyses will demonstrate the credibility of the shipboard analysis. The methods used by the shore laboratory are different as compared to the shipboard analysis and there is bound to be some variances. Such variances have to be recorded. Armed with this information, the operator can use the shipboard analysis for routine or quick checks and have a good idea of how far the results may differ from the shore lab results.

Decisions on machinery and oil maintenance should always be made with regard to the observed trend of UOA results.

5 ACKNOWLEDGEMENT

This document was made by the CIMAC Working Group Lubricants. At the time of this document's publication, the following companies are a member of the CIMAC Working Group Lubricants. For clarity, the companies are listed by their generically known names rather than their legal entities.

- Aegean Lubricants
- Alfa Laval
- BOLL & KIRCH
- Brookes Bell
- Caterpillar Motoren
- Castrol Marine
- Chevron Lubricants
- Chevron Oronite
- CMA CGM
- DNV
- ENEOS Corporation
- Exponent International
- ExxonMobil
- Gulf Oil Marine
- Hans Jensen Lubricators
- Hug Engineering
- Infineum
- INNIO Group
- IPAC
- Japan Engine Corporation
- Lloyds Register
- London Offshore Consultants
- Lubrizol
- LUKOIL Marine Lubricants
- Maersk Oil Trading Lubricants
- MAN Energy Solutions - Denmark
- MAN Energy Solutions - Germany
- National Maritime Research Institute, Japan
- Parker Hannifin
- Rolls-Royce Power Systems
- Shell
- Sinopec
- TOTAL Lubrifiants
- Viswa Lab
- VPS
- Wärtsilä
- Winterthur Gas & Diesel

Imprint

CIMAC e. V.
Lyoner Strasse 18
60528 Frankfurt
Germany

President: Prof. Dr. Donghan, Jin
Secretary General: Peter Müller-Baum

Phone +49 69 6603-1567
E-mail: info@cimac.com

Copyright

© CIMAC e.V. All rights reserved.

All contents, including texts, photographs, graphics, and the arrangements thereof are protected by copyright and other laws protecting intellectual property.

The contents of this document may not be copied, distributed, modified for commercial purposes. In addition, some contents are subject to copyrights held by third parties. The intellectual property is protected by various laws, such as patents, trademarks and copyrights held by CIMAC members or others.

CIMAC, the International Council on Combustion Engines, was founded in 1951 as a global non-profit association to promote technical and scientific knowledge exchange in the field of large internal combustion engines. CIMAC consists of National and Corporate Members from the Americas, Asia and Europe, and is supported by engine manufacturers, engine users, technical universities, research institutes, component suppliers, fuel and lubricating oil suppliers, classification societies and other interested parties. CIMAC's mission is to promote large engine technology power solutions that are efficient, reliable, safe, sustainable and of benefit to society, in pursuit of the transition to a low-carbon future.

For further information about CIMAC please visit <http://www.cimac.com>.